*BIOZEEN® We are into the business of Saving Lives



Agenda



- •Biozeen Introduction
- Stainless Steel
- •Types of Stainless Steel used in biopharmaceutical industry
- •Selection of the Stainless Steel
- •Welding in bioprocess equipment & Welding Management System
- Controlling welding
- Welding Documentation

Noble Cause, Unique Model





NOBLE CAUSE, UNIQUE MODEL





Design Build Solutions

Bioreactor systems
Fermentor systems
Process systems
CIP and SIP systems
Filtration systems
Bio-Kill systems
Sanitary Vessels
Crystallizers
Interconnection pipir



Automation Solutions

- Plant Automation
- PLC Programming
- •DCS Systems
- Automation Up gradation

PEP-PROCESS, EQUIPMENT, PEOPLE



Technology Services

- Process Design
- Process Optimization
- Contamination trouble shooting
- Process Validation
- Project Management



Research & Development

- Efficiency Improvement studies
- Glycosylation
- Perfusion with micro carriers
- Algae culture
- High cell density of VERO / CHO cell lines



Manpower Training

- Fermentation Technology
- Mammalian Cell Culture Technology
- Downstream Processing
- Sterilization & Filtration Technology
- Bioprocess Engineering
- Regulatory Aspects& Documentation



BiOZEEN Regulatory Services

- Filter TrainOptimization Study
- Compatibility Study
- Product based Integrity Study
- Bacterial Retention Study
- Protein & Preservative Binding Study

BiOZEENites

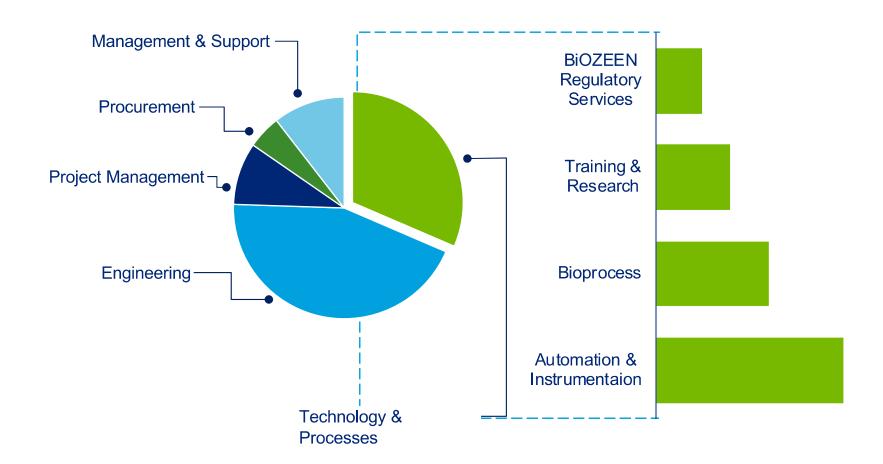


Head Quarters: Bangalore

Employees: 225

Number of Business Lines: 6

Number of Product Lines: 8







- Campus spread across 4 Hectares
- Floor area of 35,000 Sq. ft
- Executed Bioreactor/ Fermenter from 1L to 10000L

Manufacturing Workshop

In-house facility for electro polishing

- State-of-the-art Quality Control Units
- Clean and Black utilities
- Boilers, Chillers, Compressors, WFI generators

Integrated FAT centre













Manufacturing Workshop

- State-of-the-art New Manufacturing Centre located in Hardware Park, Bangalore, India
- Floor area of 50,000 Sq. ft
- Operational since June 2018





Manufacturing Workshop

- State-of-the-art New Manufacturing Centre located in Hardware Park, Bangalore, India
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Stainless Steel





The date was June 4, 1912

Harry Brearley was in charge of the Brown-Firth Research Laboratory in Sheffield, England.







While the lab was investigating ways to eliminate rust in gun barrels, Mr. Brearley noticed that a discarded steel sample from an earlier test was not rusting while the other samples rusted.

Two months later, on August 20, 1912, stainless steel was cast for the first time



Stainless Steel

Even though many people were involved in finding Stainless Steel, records consider Mr. Brearley as the inventor of Stainless Steel!

(No work is done without documentation)



A NON-RUSTING STEEL.

Sheffield Invention Especially Good for Table Cutlery.

According to Consul John M. Savage, who is stationed at Shoffield, England, a firm in that city has introduced a stainless steel, which is claimed to be non-rusting, unstainable, and untarishable. This steel is said to be especially adaptable for table cutlery, as the original polish is maintained after use, even

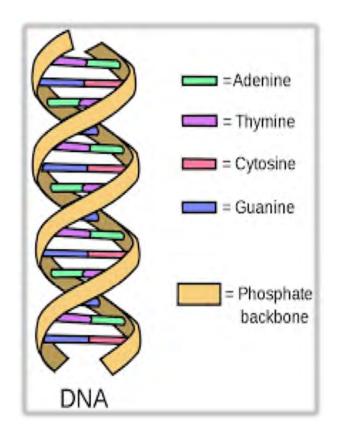
when brought in contact with the most acid foods, and it requires only ordinary washing to cleanse.

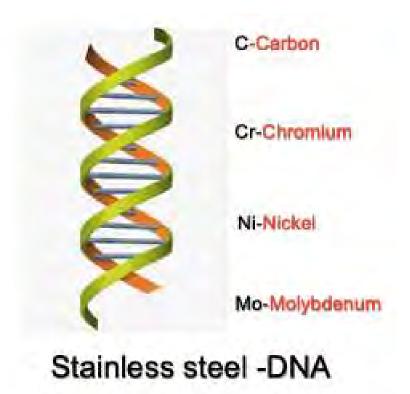
"It is claimed," writes Mr. Sayage in the Commerce Reports, "that this steel retains a keen edge much like that of the best double-sheer steel, and, as the properties claimed are inherent in the steel and not due to any treatment.

properties claimed are inherent in the steel and not due to any treatment, knives can readily be shurpened on a 'steel' or by using the ordinary cleaning machine or knifeboard. It is expected it will prove a great boon, especially to large users of cutlery, such as hotels, steamships, and restaurants. "The price of this steel is about 26 cents a pound for ordinary sizes, which is about double the price of the usual steel for the same purpose. It also costs more to work up, so that the initial cost of articles made from this new discovery, it is estimated; will be about double the present cost; but it is considered that the saving of labor to the customer will more than cover the total, cost of will more than cover the total cost of the cutlery in the first twelve month."



Today, there are 200 types of Stainless steels available.





As these 4 elements change,

- Type of stainless steel change
- Composition Changes
- Properties Changes



- <u>Austenitic:</u> High Chromium and Nickel content of the grades in this group provide superior corrosion resistance and very good mechanical properties (eg: 304, 304L,316, 316L)
- <u>Super austenitic:</u> A subgroup of austenitic stainless steels. Having elevated levels of nickel, chromium, and molybdenum compared with standard austenitic stainless steels. May have other additions (e.g., nitrogen and/or copper) to increase strength and resistance to pitting corrosion and stress corrosion cracking in the presence of chlorides. (eg: 904L(N08904), 6MO/254 SMO (S 31254), AL-6XN (N08367)
- <u>Ferritic:</u> A higher corrosion resistance than martensitic grades, but are mostly inferior to the austenitic grades. These grades are straight Chromium steels with no Nickel (eg: 409, 405,430, 444)



- Martensitic: A group of stainless alloys made to be corrosion resistant and hardenable (using heat treating). Chromium steels without nickel. Used where hardness, strength, and wear resistance are required like filter holder support and cross flow filter bars etc. (eg: 410, 420,440A, 440C)
- <u>Duplex</u>: Duplex grades are a combination of austenitic and ferritic material. Twice as strong as the austenitic and ferritic grades. Better toughness and ductility than the ferritic grades, they do not reach the levels of the austenitic grades. Duplex grades have a corrosion resistance very close to the austenitic grades such as 304 and 316. Grade 2205 is the most widely used in the duplex class
- <u>Precipitation hardening</u>: Precipitation hardening stainless steel can be strengthened and hardened by heat treatment. This offers the designer a unique combination of fabric-ability, strength, ease of heat treatment, and corrosion resistance not found in any other class of material. These grades include 17Cr-4Ni (17-4PH) and 15Cr-5Ni (15-5PH)



Table 1: Austenitic Stainless Steel Chemical Compositions (Weight Percent)

	Austenitic Stainless Steels									
Common Name	UNS No.	С	Cr	Ni	Mo	N	Mn	Cu	Other	
201	S20100	0.15	16.0-18.0	3.5-5.5	-	0.25	5.50- 7.50			
301	S30100	0.15	16.0-18.0	6.0-8.0		0.10	2.00	7		
304L	S30403	0.030	17.5-19.5	8.0-12.0	-	0.10	2.00	-	-	
305	S30500	0.12	17.0-19.0	10.5-13.0	-	*	2.00	-	-	
321	S32100	0.08	17.0-19.0	9.0-12.0		0.10	2.00		Ti 5x(C+N)	
347	S34700	80.0	17.0-19.0	9.0-13.0			2.00	-	Cb 10xC to 1.00	
309S	S30908	0.08	22.0-24.0	12.0-15.0	-	-	2.00	1.4	-	
310S	S31008	0.08	24.0-28.0	19.0-22.0		-	2.00	-		
316L	S31603	0.030	16.0-18.0	10.0-14.0	2.00- 3.00	0.10	2.00			
317L	S31703	0.030	18.0-20.0	11.0-15.0	3.0-4.0	0.10	2.00	-	-	
317LMN	S31726	0.030	17.0-20.0	13.5-17.5	4.0-5.0	0.10-0.20	2.00	-	-	
904L	N08904	0.020	19.0-23.0	23.0-28.0	4.00- 5.00	0.10	2.00	1.00-2.00		

Table 2: Common Ferritic Stainless Steel Chemical Compositions (Weight Percent)

	Ferritic Stainless Steels										
Common Name	UNS No.	C	Cr	Ni	Mo	N	Mn	Cu	Other		
409	S40910	0.030	10.5-11.7	0.50	-	0.030	1.00	-	Ti 8x(C+N) to .50 Cb 0.17		
	S40920	0.030	10.5-11.7	0.50		0.030	1.00		Ti 8x(C+N) min. Ti 0.15-0.50 Cb 0.10		
	S40930	0.030	10.5-11.7	0.50	•	0.030	1.00	3	(Ti+Cb) [0.08+8x(C+N)] to 0.75 Ti 0.05 min.		
405	S40500	0.08	11.5-14.5	0.60	-	-	1.00	-	Al 0.10-0.30		
430	S43000	0.12	16.0-18.0	0.75	-	-	1.00	-	-		
434	S43400	0.12	16.0-18.0		0.75- 1.25	•	1.00	-	-		
438	S43800	0.12	16.0-18.0	•	0.75- 1.25	•	1.00		Cb 5xC to 0.80		
439	S43035	0.030	17.0-19.0	0.50	-	0.030	1.00		Ti [0.20+4(C+N)] to 1.10 Al .15 max.		
444	S44400	0.025	17.5-19.5	1.00	1.75- 2.50	0.035	1.00		(Ti+Cb) [0.20+4(C+N)] to 0.80 max.		
26-3-3	S44660	0.030	25.0-28.0	1.0-3.5	3.0-4.0	0.040	1.00	-	(Ti+Cb) 0.20 to 1.00 and (Ti+Cb) 8x(C+N) min.		

Table 3: Common Martensitic Stainless Steel Chemical Compositions (Weight Percent)

Martensitic Stainless Steels									
Common Name	UNS No.	C	Cr	Ni	Mo	N	Mn	Cu	Other
410	S41000	0.08-0.15	11.5-13.5	0.75	-		1.00	-	
420	S42000	0.15 min.	12.0-14.0	0.75	0.50	•	1.00		•
440A	S44002	0.60-0.75	16.0-18.0	-	0.75		1.00	-	-
440C	S44004	0.95-1.20	16.0-18.0	-	0.75		1.00	-	



Table 4: Common Precipitation Hardening Stainless Steel Chemical Compositions (Weight Percent)

Precipitation Hardening Stainless Steels									
Common Name	UNS No.	С	Cr	Ni	Мо	N	Mn	Cu	Other
XM-13	S13800	0.05	12.3-13.2	7.5-8.5	2.00-2.50	0.01	0.20	-	AJ 0.90-1.35
XM-12	S15500	0.07	14.0-15.5	3.5-5.5			1.00	2.5-4.5	Cb+Ta 0.15-0.45
632	S15700	0.09	14.0-16.0	6.5-7.7	2.00-3.00	•	1.00	-	Al 0.75-1.50
630	S17400	0.07	15.0-17.5	3.0-5.0			1.00	3.0-5.0	Cb+Ta 0.15-0.45
631	S17700	0.09	16.0-18.0	6.5-7.7	-	-	1.00		AJ 0.75-1.50



Table 5: Common Duplex Stainless Steel Chemical Compositions (Weight Percent)

Common	UNS No.	C	Cr	Ni	Mo	N	Mn	Cu	Other
Name									
	S31200	0.030	24.0-26.0	5.5-6.5	1.20- 2.00	0.14-0.20	2.00	•	•
	S31260	0.030	24.0-26.0	5.5-7.5	2.5-3.5	0.10-0.30	1.00	0.20-0.80	W 0.10-0.50
	S32001	0.030	19.5-21.5	1.00-3.00	0.60	0.05-0.17	4.0-6.0	1.00	
	S32003	0.030	19.5-22.5	3.0-4.0	1.50- 2.00	0.14-0.20	2.00	-	+
	S32101	0.040	21.0-22.0	1.35-1.70	0.10-	0.20-0.25	4.0-8.0	0.10-0.80	
	S32202	0.030	21.5-24.0	1.00-2.80	0.45	0.18-0.26	2.00	-	
2304	S32304	0.030	21.5-24.5	3.0-5.5	0.05- 0.60	0.05-0.20	2.50	0.05-0.60	-
2205	S31803	0.030	21.0-23.0	4.5-6.5	2.5-3.5	0.08-0.20	2.00	-	-
2205	S32205	0.030	22.0-23.0	4.5-6.5	3.0-3.5	0.14-0.20	2.00	-	
	S32506	0.030	24.0-26.0	5.5-7.2	3.0-3.5	0.08-0.20	1.00	-	W 0.05-0.30
	S32520	0.030	24.0-26.0	5.5-8.0	3.0-4.0	0.20-0.35	1,50	0.50-2.00	
255	S32550	0.04	24.0-27.0	4.5-6.5	2.9-3.9	0.10-0.25	1.50	1.50-2.50	-
2507	S32750	0.030	24.0-26.0	6.0-8.0	3.0-5.0	0.24-0.32	1.20	0.50	
	S32760	0.030	24.0-26.0	6.0-8.0	3.0-4.0	0.20-0.30	1.00	0.50-1.00	W 0.50-1.00
	S32808	0.030	27.0-27.9	7.0-8.2	0.8-1.2	0.30-0.40	1.10	-	W 2.10-2.50
	S32906	0.030	28.0-30.0	5.8-7.5	1.50- 2.60	0.30-0.40	0.80-1.5	0.80	
	S32950	0.030	26.0-29.0	3.50-5.20	1.00- 2.50	0.15-0.35	2.00	-	
	S39274	0.030	24.0-26.0	6.8-8.0	2.5-3.5	0.24-0.32	1.0	0.20-0.80	W 1.50-2.50
	S82011	0.030	20.5-23.5	1.0-2.0	0.10- 1.00	0.15-0.27	2.0-3.0	0.50	-



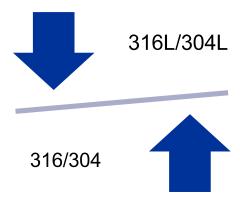
Summary of the main advantages of the stainless steel types

Туре	Examples	Advantages	Disadvantages
Ferritic	410S, 430, 446	Low cost, moderate corrosion resistance & good formability	Limited corrosion resistance, formabilty & elevated temperature strength compared to austenitics
Austenitic	1304 316	Widely available, good general corrosion resistance, good cryogenic toughness. Excellent formability & weldability	Work hardening can limit formability & machinability. Limited resistance to stress corrosion cracking
Duplex	1.4402	Good stress corrosion cracking resistance, good mechanical strength in annealed condition	Application temperature range more restricted than austenitics
Martensitics	420, 431	Hardenable by heat treatment	Corrosion resistance compared to austenitics & formability compared to ferritics limited. Weldability limited.
Precipitation hardening	11//4PH	Hardenable by heat treatment, but with better corrosion resistance than martensitics	Limited availability, corrosion resistance, formability & weldability restricted compared to austenitics



Types of Stainless Steel – Product Contact

- Type 316:
- 18% chromium, 14% Nickel and added Molybdenum
- In combination increase its resistance to corrosion.
- In particular, molybdenum helps to control the pit type attack of corrosion.
- The "L" grades provide extra corrosion resistance **after welding**. (Carbon levels are kept to .03%)



Types of Stainless Steel – Product Contact Surface

• Type 316L (1.4435):

Slightly higher

- (17.0to19.0%) chromium,
- (12.5 to 13.5% Nickel) and
- (2.5 to 3.0%) Molybdenum.
- This grade stainless steel helps in control of delta control at the welding area.
- (outcome of the Basler Norm 2 that tried to reduce concerns of rouging)



Select the Right Stainless Steel

How do we select the right one for our application?

- Corrosive environment: Atmospheric, water, concentration of particular chemicals, chloride content, presence of acid
- Temperature
- Strength Required
- Metal Joining Process Required
- Degree of Forming Required
- Product Form Required
- Surface Finish Required
- Cost

When in doubt, please share the process details & chemicals that come in contact to the manufacturer to check the compatibility.

Stainless Steel Welding



Stainless Steel Welding

For pressure vessels, tanks, piping and tubing systems where the process contact surface of the weld is to be used "As is",

- welding processes shall be limited to the inert-gas arc processes (such as gas tungsten-arc welding and plasma arc welding)
- the high energy beam processes (such as electron beam or laser beam welding), as defined in AWS A3.0







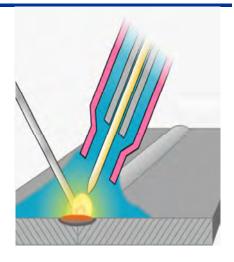


Gas Tungsten Arc Welding

Joining of metal by placing an arc in between the metals Shielding with an inert gas or mixture.

With or without filler material

Manual or automatic (orbital welding)









Weld Controlling

S-Sulphur control in Steel

O-Oxygen control in Welding Gas

F-Ferrite control in Steel

T-Tungsten control in process



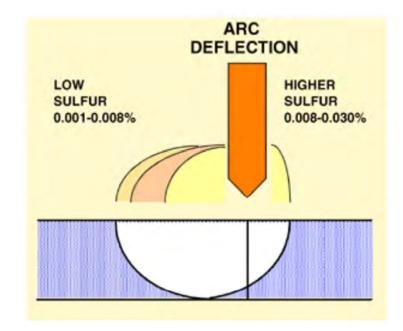
Weld Controlling - Sulphur

MM-5.2.1.1 Weld Ends.

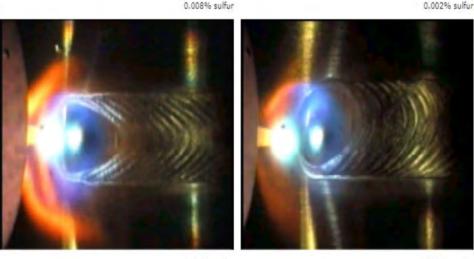
Weld ends that are to be automatically welded shall have a Sulphur content between 0.005 wt. % and 0.017 wt. %

This requirement applies to the austenitic stainless steels

This requirement does not apply to materials used in the construction of process components, only to the weld ends of process components in their final form.



Frames from an AMI in-house video showing lathe welds of 316L tubing using Arc Machine's arc filtration system to view the weld pool, Leftr. Weld of 0.008% to 0.008% sulfur with symmetrical weld puddle. Right, Weld of 0.002% sulfur (top) to 0.014% sulfur. Note asymmetrical puddle, Electrode is centered on the weld joint, while the weld puddle is offset towards the low sulfur heat. Henon, unpublished data.



0.008% sulfur

0.014% sulfur



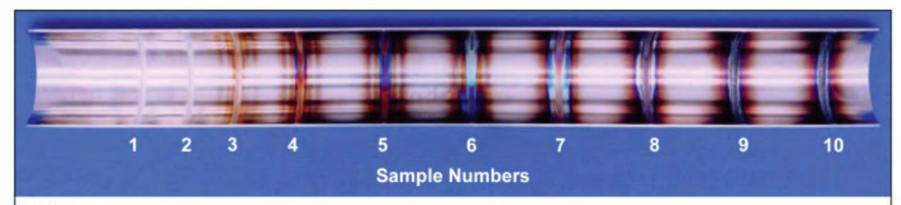
Weld Controlling - Sulphur





Weld Controlling - Oxygen

Oxygen contamination during welding leads to Discoloration and corrosion!



Notes:

1. The tube sample was prepared by making ten autogenous welds on the outside diameter of a 2 in. (50.8 mm) 316L stainless steel tube. Welds on 304L tubing showed no significant difference in heat tint from 316L. The welds were full penetration welds. The torch shielding gas was 95% argon, 5% hydrogen [99,998 with <2 parts per million (ppm) of oxygen, moisture, and hydrocarbons] to assure full penetration welds. The hydrogen addition to the torch shielding gas is considered to have no effect on the HAZ heat-tint oxide on the inside surface. To provide varying amounts of oxygen in the backing gas a compressed cylinder of medical grade air was added to 99.98% minimum pure argon (<2 ppm of oxygen, moisture, and hydrocarbons) and the oxygen was measured with a calibrated commercial oxygen indicator. The amount of oxygen in ppm in the backing gas was measured to be as follows:</p>

No. 1-10	No. 3-50	No. 5-200	No. 7-1000	No. 9-12500
No. 2-25	No. 4-100	No. 6-500	No. 8-5000	No. 10-25000

The illustration should be used as a reference to identify the degree of heat-tint oxide by number and not to specify oxygen limits in the backing gas.
 The acceptable degree of heat tint can vary with different service environments. It should be considered along with the economics involved obtaining very low levels of heat tint when specifying acceptable heat tint level welds.

The amount and visual appearance of heat-tint oxide can be influenced by factors other than oxygen, such as:

- High levels of moisture in the backing gas will increase the degree of heat-tint.
- Contaminates such as hydrocarbons, moisture, and some types of particulate on the surface prior to welding can influence heat-tint oxide levels.
- Hydrogen gas in the argon backing gas can significantly reduce the amount of heat-tint oxide.
- The metal surface finish can have a varying affect on the visual appearance of heat tint.

Figure 10. AWS D18.2 weld discoloration chart.



Weld Controlling - Oxygen

Oxygen contamination during welding leads to Discoloration and corrosion!



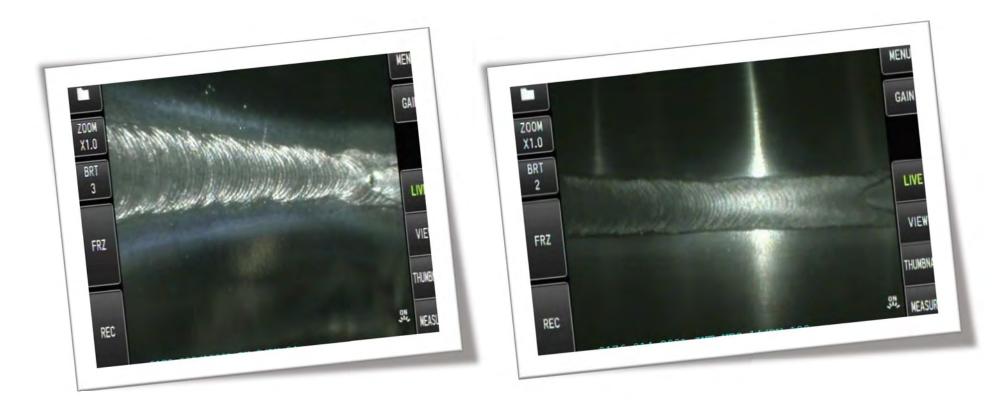






Weld Controlling - Oxygen

Oxygen contamination during welding leads to Discoloration and corrosion!



Without Oxygen Monitoring

With Oxygen Monitoring



Weld Controlling – Delta ferrite

Ferrite is a phase that may precipitate during solidification of austenitic stainless steel depending on the ratios of the alloying elements.

The presence of ferrite in austenitic stainless steel welds may reduce the corrosion resistance in some corrosive environments.

However, a minimum ferrite level may be required to maintain specific properties of particular product forms (e.g., castings) or is deemed necessary to prevent hot cracking of heavy wall weldments (e.g., vessels made from plate).

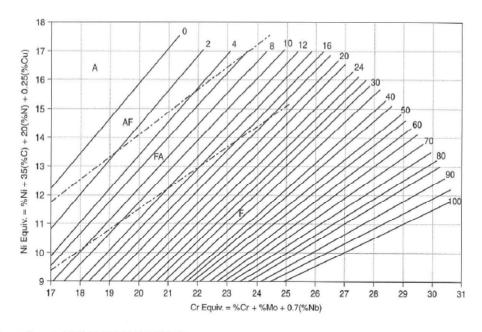
The ferrite level of as-solidified austenitic stainless steel welds can be determined from the WRC-1992 Constitution Diagram for Stainless Steel Weld Metals using

- Chromium equivalent Cr (eq) p %Cr + %Mo + 0.7%Nb and
- Nickel equivalent Ni (eq) p%Ni + 35%C + 20%N + 0.25%Cu.

Measuring of ferrite in production welds shall be in accordance with AWS A4.2M:2006 (ISO 8249:2006MOD).



Weld Controlling - Deltaferrite



Source: Figure 1 of AWS A5.9/A5.9M:2006 ERRATA

Figure A.1—WRC-1992 Diagram for Stainless Steel Weld Metal

The WRC-1992 Diagram predicts ferrite in Ferrite Number (FN).

The WRC 1992 Diagram is preferred for "300" series stainless steels and for duplex stainless steels. It may not be applicable to compositions having greater than 1% Si



Weld Controlling – Delta ferrite

Ferrite in welds of austenitic stainless steels can be controlled by one or more of the following methods:

- (a) Post weld solution annealing
- (b) Use of weld filler with increased nickel content
- (c) Increase of nickel equivalent by addition of approximately 1–3 vol.% nitrogen to shielding gas
- (d) Selection of heats of materials with high nickel to chromium ratios, such as the European steel grade
- 1.4435 (see Table MM-2.1-1) with a restricted Cr(eq) to Ni(eq) ratio 3 as per BN2



Weld Controlling – Delta ferrite

The Basler norm 2 (BN2) describes the special material requirements of 1.4435 according to DIN 17440 with clearly narrowed analysis limits for the alloy components and defined ferrite content (ferrite).

Target delta ferrite is 3% at weld joint

Table MM-5.2.1.2-1 Predicted Ferrite Number (FN) Ranges for Various Austenitic Stainless Steel Product Forms and Welds

Product Form	Expected FN				
Wrought product forms with sulfur levels less than 0.005%	0.5 to 4				
Wrought product forms with a sulfur range of 0.005% to 0.017%	1.0 to 6				
GMAW/GTAW using E316L [Note (1)]	4 to 12 [Note (2)]				
SMAW using ER316L [Notes (3), (4)]	4 to 10 [Note (5)]				
CF8M and CF3M castings	5 to 15				



Weld Controlling – Delta Ferrite

Ferritoscope

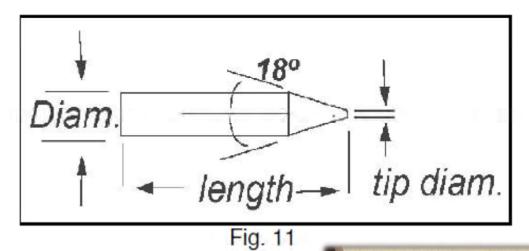






Weld Controlling - Tungsten

Angle and profile of tungsten electrode is critical to maintain the weld bead width & profile









Weld Controlling – Welder

- Welding Management System
- Certified Skilled Welder
- Welding Procedure
- Welder Qualification
- Weld Coupons before job



Uniqueness of Welding Operation

- Successful operation for obtaining defect-free welds ("sound") is largely determined by the welders' skill – called "Eye-Hand Motor- Coordination [EHMC]"
- The welder is a human being & hence subject to individual variability in traits & behaviors – eg, discipline, temperament, etc
- A large number of other engineering or technical factors need to be considered & planned in advance of the actual welding operations



Other Unique features

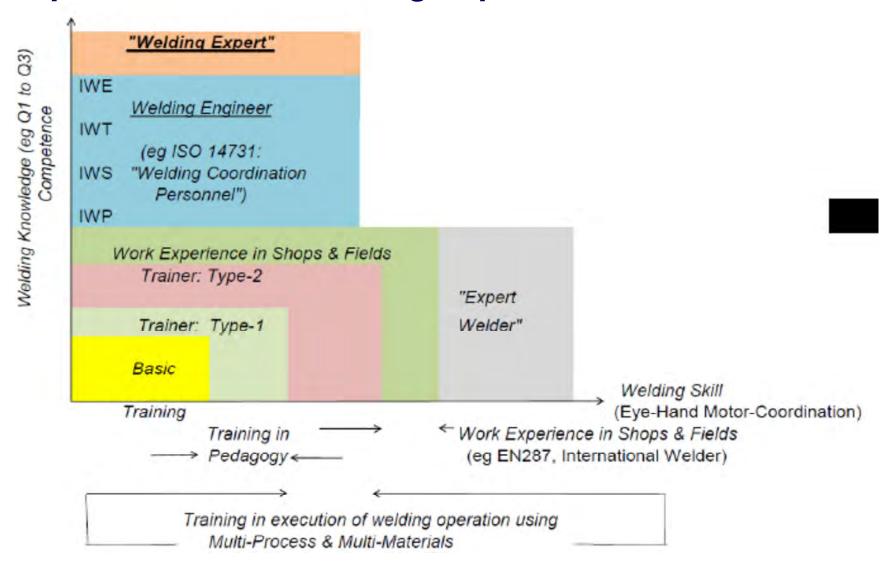
- "Performance" of even the most "sound weld" during service can never be pre-determined but has to be assumed using corroborative inspection-reports, interpreting testing-results, judicious analysis, & good engineering judgment using experience gained from similar applications
- Un-predictability of "Distortion" is unique to welded structures, in that no other process introduces such critical un-certainty; causing serious delays, damages, or very costly rejections
- A wide range of "Welding Processes" are available & need to be carefully evaluated for the specific application; the most common ones for welding steel are: MMAW, TIG, MIG, SAW, Resistance, Stud, etc



Quality of Weld Vs Performance of Weld

- These two terms are often mixed-up & needs clarification here
- Quality of the weld refers to its "sound-ness" ie "freedom from defects"
- "Performance" refers to how well the weldment discharges its designed function under the service conditions that it encounters during its life-time
- Therefore, while quality of welding is <u>ESSENTIAL</u> to contribute to its performance in service, it is <u>NOT</u> <u>SUFFICIENT</u> to ensure it!!

Expert Welder Vs Welding Expert







WPS, SWPS, WPQT

- The Welding Procedure Specification [WPS] is the heart of the Weld Management System [WMS]
- WPS is a document which un-ambiguously prescribes all necessary details which enable the execution of the welding operation
- SWPS is a standardized form of WPS which has been proved by a reputed 3rd party & hence is allowed to be used without qualification testing [WPQT]



Moving Forward.....

- Welders are certified on the basis of their skill-competency for executing qualified welding procedures [WPS] using a standardized set of variables
- These qualified WPSs need to be be validated to suit the job
- The WPS is qualified thru mechanical testing to meet the structural strength & ductile-failure criteria called "designperformance", while the WPQ is tested for "soundness" or "quality"
- The Rules governing such qualifications are universally adopted by industry worldwide thru Codes & Standards (eg ASME BPV Sec IX & ISO 1561X



Welding variables

- These are the specific inputs, values or factors which determine the outcome of the weld – either design-performance, soundness, or otherwise
- If all variables in the WPS are controlled during the execution of welding, the weldment can be expected to perform as designed

Welding "variables" to be managed during the Opertion

- SUC: Set-Up Conditions ie how the different parts are juxtaposed against each other at the joint <u>prior to</u> <u>start</u> of welding
- SWIP: Sequence of Welding & Inspection Plan ie the detailed <u>step-by-step actions</u> to realize the weld – including inspection stages & post-weld operations
- RPC: Recommended Parameters Chart- ie what values of operating conditions of the Process to use <u>during</u> welding

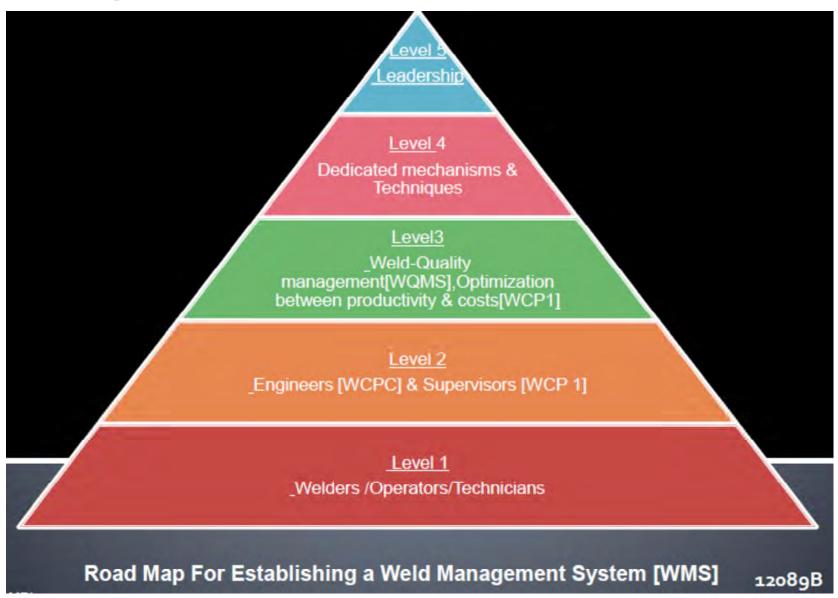


Welding "Aspects" to be managed

- What about those factors which are to be planned <u>in</u> <u>advance</u> of the operation?
- Even if the skill-of-welding is to be eliminated thru a Robotic Arm, a lot of due diligence is required for selecting the right one for the application, & planning for procurement, installation & integration into manufacturing are required
- These need to be organized well in advance of the actual welding operation



Road Map





Welding GAP Audit

The welding requirements of the Organization are closely scrutinized & compared wrt the mapping of its:

- Current disposition of technology, practices, people, systems, etc
- State of preparedness to meet its desirable futurestate

The Top Management of the Organization supports this review by being closely associated with the Welding-Gap Audit



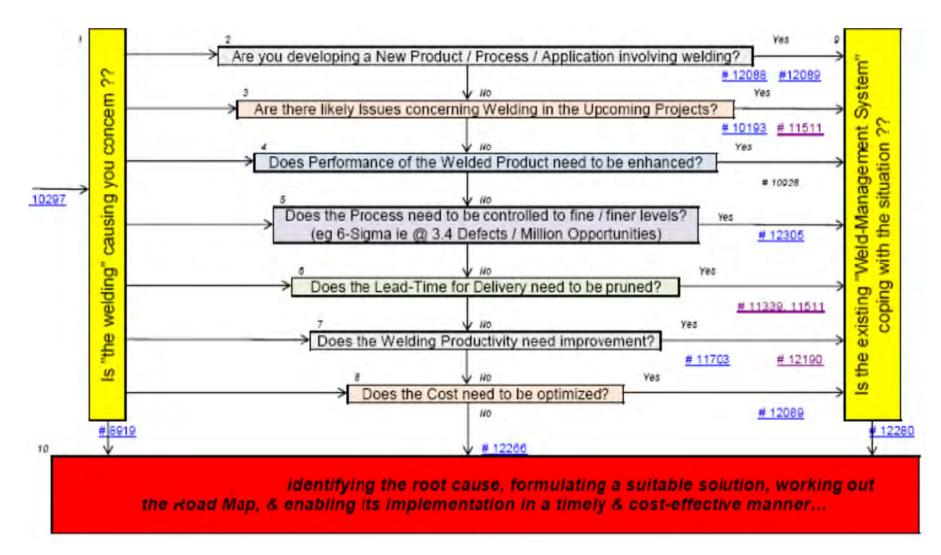
Welding GAP Audit

- The starting point is a self-assessment by the Top Management on the current dispositions & the aspirations of the Organization
- The Report with its Recommendations are used as the basis for charting out an Overall Road Map for establishing the WMS



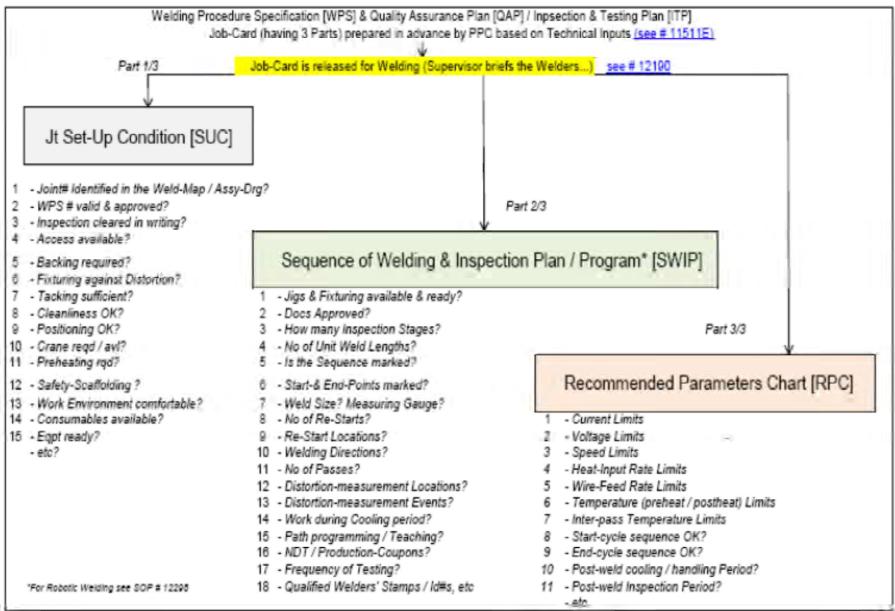
Welding GAP Audit

<u>De-Burden your Welding !!</u>





Qualifications





Welding Management System Overall Road Map

- This is a basic Project-Plan Document which divides the work into Phases, bifurcates the scopes & identifies the Key Change Agent
- The Project Manager & Project Leader are identified
- The Project Manager prepares the ORM



Welding Management System Detailing Road Map

- This is jointly prepared by the Team Leader & the Project Manager
- In addition to detailing the above, it specifies the budgets, resources, schedules, re-structuring & reorganization, etc
- This detailed project plan is broken down into tasks ("Work Breakdown Structure")
- Broad phases for implementation are given in the next slide



Stages of implementation of WMS

- Establish the Top-Down "Organizational Framework" linking all the processes in the welding-functional chain for the product
- Establish the Guidelines for Contract Review as related to Welding
- Establish the Communication Sub-System, starting with Drgs released from the R&D / Design thru Mtls, SWIPs for Welders, etc, thru Insp & back to Mgmnt
- Establish the traceability-routes for materials, consumables, processes, etc.
- Establish the WPS, WPAR, WPQ, Sub-Systems; qualify the welders to meet the demand of skill-competency
- Deploy the skills according to the MATRIX
- Verify the performance from Service & feedback from Customer / User
- Document all the above processes; review & improve



Welding Management System Practising WMS

- After establishing the above processes, run thru the system for several cycles / iterations for all critical / identified jobs over a pre-determined period of time
- Track the history, experiences, feedbacks, etc, & update the documentation
- Improve & scale up in a calibrated manner to cover all the job-orders (or pre-determined %, as appropriate for the level of control – ie ISO 3834-2, 3, OR 4)
- When ready, apply for Certificate to Manufacturer's Certification Body for Audit to ISO 3834 (or as appropriate)



Welding Management System Concluding WMS

- The WMS can be implemented in any Organization where welding plays a critical role
- The Organization can implement it systematically well in advance of actually executing major project-orders
- The Welding-Gap Audit is the basic 1st step in implementation of WMS
- Road Maps for successfully establishing the WMS can be formulated to suit the Organization's needs

Welding Controlling



Weld Controlling – NDT

Radiography Inspection



■ Dye Penetrant Test



Borescope





















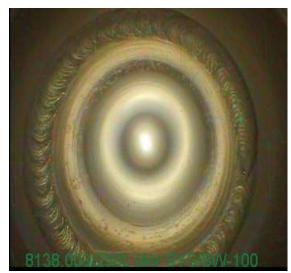
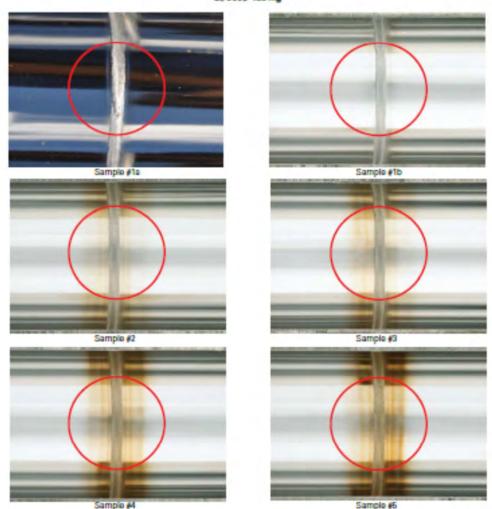




Fig. MJ-8.4-2 Discoloration Acceptance Criteria for Welds and Heat-Affected Zones on Electropolished UNS \$3 1603 Tub ing



The weld backs shown in the above photographs are the weld breads on the LD, of the tubing. The area for comparison in each photograph is the area inside the end droke. The weld back shall have no discoloration. Weld heat-affected sones on electropolished UNS 531603 tubing with discoloration levels no worse than Samples #1 through #4 in the sax-welded condition are acceptable. Heat-affected sone discoloration levels more severe than that shown in Samples #4 are unacceptable. Sample #5 shows unacceptable weld and heat-affected sone discoloration levels for comparison. The user is cautioned that the colors observed during direct visual examination or borescope examination will be different viewing directly down (90 deg) at the surface compared with viewing at a lower angle along the edges.

GENERAL NOTE: The user is ocutioned that electronic versions or photocopies of these acceptance criteria shall not be used for evaluation of sample or production welds since subtle differences in color can influence weld a coeptability. Nonmandatory Appendix M explains the technique by which these acceptance criteria were determined.

This figure is also available as a stand-alone document from ASME as ASME BPE-EP.



Equipment Name: Equipment Model No:

CHECKLIST FOR MANUFACTURING DOCUMENTATION OF BIOPROCESS EQUIPMENTS



SEPARATE FILE: TESTING INSTRUMENTS CERTIFICATES (from supplier + BZ)

	Calibration certificate for Ra meter standard piece
- 1	Calibration Certificate for Gauges used for PHT
	Calibration Certificate for measuring Instruments (tape / caliper / level)



Filler Rod Certificate

NO	CUSTOMER	: BEN	: BENAKA INDUSTRIAL PRODUCT GRADE:								ER-316L/1.4430			
	INVOICE NO.	: 4569	: 4569/2018-2019									HEAT NO : V13129		
PRODUCT	PRODUCT FORM	: STA	: STAINLESS STEEL WELDING WIRE.											
PRODU NFORM	DIMENSION	: 2.40	: 2.40mm Tol :- ±0.05mm											
=	IDENTIFICATION	; BOX	; BOX NO.; HH 01-8 QUANTITY : 200 KGS											
	CONDITION	: BRIGHT DRAWN & CUT LENGTH (1000 MM).												
7	ELEMENTS	C%	Si%	Mn %	P%	S%	Cr%	Ni %	Cu%	Mo %	N%	Nb%	Ti%	
CHEMICAL	SPECIFIED MIN MAX	0.03	0.65	1.00 2.50	0.03	0.02	18.00 20.00	11.00 14.00	0.50	2.50 3.00				
COMP	RESULTS	0.019	0.42	1.70	0.026	0.008	18.50	11.16	0.26	2.57				
			MEC	HANICA	LPROP	ERTIES	OF WEI	D MET	L(All V	(eld)				
RESULTS		N/mm ² VS (0.2%)			R.A	%	ELON	NGATIO	N %					
		577	_	430		-			40.00	+	-	+	_	

Argon Gas Certificate

Sl.No.	BGL Cylinder No.	Hydrogen
1	BGL13680	2.07 %
2	BGL1530	2.08 %
3	BGL1607 /	2.07 %
4	BGL12259	2.06 %
5	BGI.20746	2.07 %
6	BGL22081	2.07 %
7	BGL2371	2.06 %
8	BGL24347/	2.06 %
9	BGL24380	2.06 %
10	BGL24393	2.07 %

Impurities:-BGL1607 - CH4<0.10 PPM

The Concentration of Impurities in this mixture AHM 98:2 are O2<1.0 ppm. H20<1.0 ppm and dew point 76°C. The Concentration of Argon on AHM is 98.0 %.

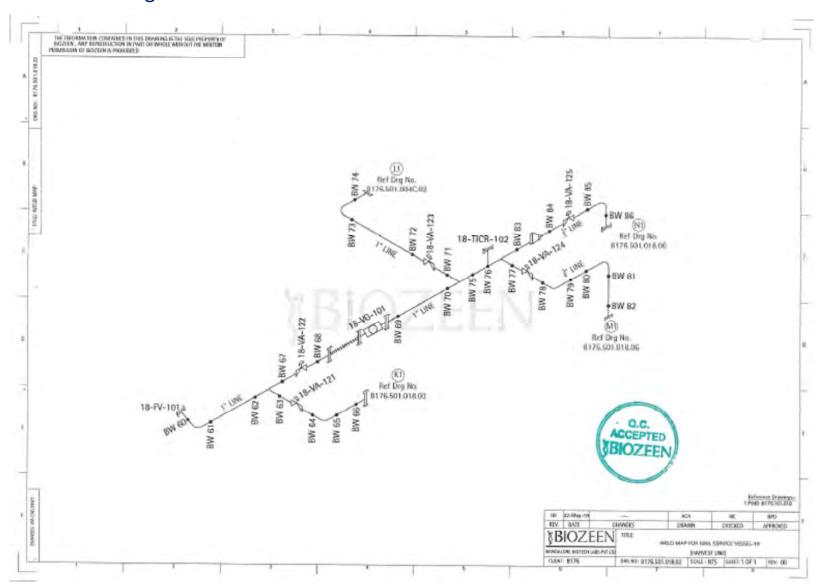
Remarks: Raw Material Purity – Hydrogen (99.999 %) & Argon (99.9995 %). Impurities of raw materials are O2<2.0 ppm, H2O<2.0 ppm and THC<0.5 ppm.

Traceability Certification:

- The Product is prepared by using Weight/Pressure Gauge of Accuracy Traceable to National Standards Through Regional Reference Standard Laboratory (Weights and Measures) Govt. of India.
- 2. The Product is certified using Reference Standard Traccable to NIST/NPL.
- Process Traceability complying with ISO 9001:2015 Certified System.



Weld Isometric Diagram





Weld Log

FORMAT NO:BBL/ENGG-QC/R/WEL.001/R02



					WELD	LOG	- Ha	ave	st Line				
Project No.	1 8	176								yster	m; <u>s</u>	OOL SER	WEE WESTEL- IS
Weld Map No.: 8176 501 018 01 L4 05		Welding Gas: AHM					Welding Procedure: 008,211						
P & ID No. :	317	D 10	1 212	Shielding Gas: All	M								
	Welding Procedure				Welding		Inspection		Checked by	Accepted			
Weld no.	Marsual	Orbital	Description	Heat no/Lot no:	Date	Welder ID/Sign	Вогожоре	mage captured	Walding Inspector & Date	Yes	No.	Action	Bernarka
Bw 60	_	1	1"81 3161 0160 W	82-VI- 825/8-19	29 APR	HIT BE	~	_	24 APRZOIY	-			
			1'11 3161 clhop	469A	27 APR	MAB			8				
BW 61		1	171 3161 ppe	425F	R017		4	~	ZTAPRING	1	~		
BW 62		-	1751 3161 P. De	H25F	≥9.4PR	いりを	1		g.				
			unequal The xx 1;	848700/Y848	P105	HT	-		27 APR 2019	4	~		
BIN 63	v	-	Dia Briagen yolve 1/2 Ps	248146 A TH	30 APR	Same?	4	1	BOAFRED	1		-	
BW 64			Diaphragm value 1/2" PS	748146 ATK	30 APR	HIT		,	1				
810 64	-		1/2" SS 3161 Elbow	208575	5196	Younge "	~	1	30 APR 2019	-	-		
BIN 65	-	-	1/2" SS 3164 G(600	208575	30 APR	MIT	2		1	5			
1900	-	_	"12" IS BIEL DIPE	547422	Sold	4	-	_	30APR 2017				
BIN 66	-	-	1/2" SS 316L PIPE 1/2" TE x 1/2" PS	547422 Bz-VI-827/184	20 APR 2019	4	1	_	ZOAPR MA	1	è	-	
	1		unequal Tex 1" x 1/2"	848700/7848	BOAPR	WT			Ju .				
13W 67		-	Diaphrages value 1" PS	441035 ALF	2019	Hermal	1	1	30 APR 2019	1	-		
BW 68	-	-	Dia phragm value 1"PS	441035 ALR	ZTAPR	W74	1		8-	2		-	
500			11/2" TC X 1" PS	BZ-41-825/1519	200 AOR	-	Υ.		29 APRZNIA	4			
Bw 69	-	1	1" TC X 1"PS	425F	Z4 APR	MAR	1	_	27.498200	1	-	-	-

8176.018 500L SERVICE VESSEL - 18



Traceability and Identification





Weld Printout

		ı	001 O.S Pg (Number]1	
		U (V)	I (A)	V rot (mm/min)	
		(4)	(11)	China in 1117	()
	5s	0.4	0.2		0
	10s	0.3	0.3		0
	15s	0.4	0.2		0
S01	10	10.9	49.9	21	
		10.2	17.1		
	10°	10.8	49.9	90	0
		10.2	17.1		
	20°	10.9	49.9	90	0
		10.5	17.1		
	30°	11.0	49.9	90	0

440°	9.6	22.3	90	0
17	10.3	10.6		
451°	10.0	18.9	90	0
	10.9	9.2		
460°	10.8	15.6	90	0
	11.4	8.5		
470°	11.3	13.6	90	0
	12.5	7.5		
480°	11.8	10.3	90	0
	12.9	6.6		
491°	13.1	7.4	90	0
	13.9	5.7		
			<<<<<<	
Cycle star	t: S	at 09 M	ar 2019 00:	24:17
Cycle time	: 00	:01:18	N = 495	
>>>>>>	! We	d comme	ents! <<<	******
BIOZEEN_W1	6.8176	5.010.70	10L.AV-10	
BW-350	P			
00	4		-	
64	N	a	2019	



Welder Qualification

Welder Qualification Designation

BS EN ISO 9606-1 141 PBW FM5 S t1.65 H-L045 ss gb

WPS-Reference: 004 Rev.01 Welder's Name. Mr. Mansoor Pasha

identification: W12

Method of Identification: Company Identification

Date and place of birth: 01-01-1985 & Near Bangalore, Kamataka, India.

Employer:

M/S, Bangalore Biotech Labs Pvt.Ltd BS EN ISO 9606-1 : 2017 Code / Testing standard:

Remark: None Job knowledge: Acceptable



	Weld test details	Range of approval
Welding process(es)	TIG(141)	TIG(141)
Transfer Mode	NA.	NA.
Product type (plate or pipe)	T	T
Type of weld	BW	BW
Joint type	P BW ss gb	P BW ssmb , P BW bs, P BW ssgb
Parent Material group(s)/subgroups	ISO CR 15608 Group 8.1	ISO CR 15608 Group 8.1
Filler material group (s)	FM5	FM5
Filler material (Designation)	Solid (S)	Solid (S) , Metal Cored (M)
Shielding gas	Argon: Hydrogen Mixture(or equivalents) EN ISO 14175 : AHM	Argon: Hydrogen Mixture (or equivalents) EN ISO 14175: AHM.
Auxiliaries (e.g. backing gas)	Argon: Hydrogen Mixture(or equivalents) EN ISO 14175 : AHM	Argon: Hydrogen Mixture (or equivalents) EN ISO 14175: AHM.
Type of current and polarity	DCEN	DCEN
Waterial thickness (mm)	1.65	1.65 to 3.3.
Deposited thickness (mm)	NA	NA
Outside Pipe diameter (mm)	OD 50.8	00 ≥25.4mm.
Welding position(s)	H-L045	PA , PC , PE , PF
Weld detalls Multi-layer/single layer	(ss, gb)	(ss, gb), (ss, mb), bs

Additional information: available in WPS 004

Type of qualification tests	Performed and accepted	Not tested
Visual testing	⊠	
Radiographic testing	⊠	
Macroscopic examination		⊠
Fracture test	0	⊠

Name of the Examiner: D. SUNDARESAN Date of issue Signature of Examiner

BANGALORE 26/04/2018





Welder Qualification



QW-484A - WELDER PERFORMANCE QUALIFICATION (WPQ)

(See QW-301, Section IX, ASME Boiler and Pressure Vessel Code)



: 1.65 mm

Thickness

Welder's name: Mr. Mansoor Pasha

Test Description
Identification of WPS followed: 011 Rev 00 DT 04.01,2017

Specification and type/grade of Base Metal :

ASME SECII PART A.ED.2015 ASTM A 270/SA 213/SA213M

TYPE 316L

Testing Condition and Qualification limits

Welding variables (QW-350) Actual values Range Qualified Welding Process GTAW GTAW
Type Manual Manual

 Backing
 Without Backing
 With or Without Backing

 Plate or Tube
 Pipe (OD12.7mm)
 Plate & Pipe (OD ≥ 12.7mm)

 Base metal P- Number to P- Number
 P8 to P8
 P1 thro P15F, P34, P41 Thro P49

Filler metal or Electrode specification None None
Filler metal or Electrode Classification None None
Filler Metal F Numbers None None
Consumable Inserts (GTAW or PAW) None None
Filler type (solid/metal or flux cored/powder) None None

Deposit thickness for each process 1.65 mm 1.65 mm
Position(s) 6G All
Vertical Progression (uphill or downhill) Downhill Downhill

Type of fuel gas (OFW) NA NA
Inert gas backing (GTAW, PAW, GMAW) AHM (Argon 98% & Hydrogen 2%) AHM (Argon 98% & Hydrogen 2%)

GTAW current type DCEN DCEN



Weld Coupon





ÿBiOZEEN

References

- ASME BPE 2016
- https://www.nickelinstitute.org/media/1702/highperformancestainlesssteels 11021 .pdf
- Guidelines for the welded fabrication of nickel-containing stainless steels for corrosion resistant services Nickel Development Institute o Reference Book, Series N 11 007
- DESIGN GUIDELINES FOR THE SELECTION AND USE OF STAINLESS STEEL Nickel Development Institute o Reference Book, Series N 9014
- ASME Section VIII (Rules for Construction of Pressure Vessels)
- ASME Section IX (Welding, Brazing & Fusing)
- ASME Section II (Materials)

Thank You!